

*ELEC0047 - Power system dynamics, control and stability*

## Dynamic simulation of a five-bus system

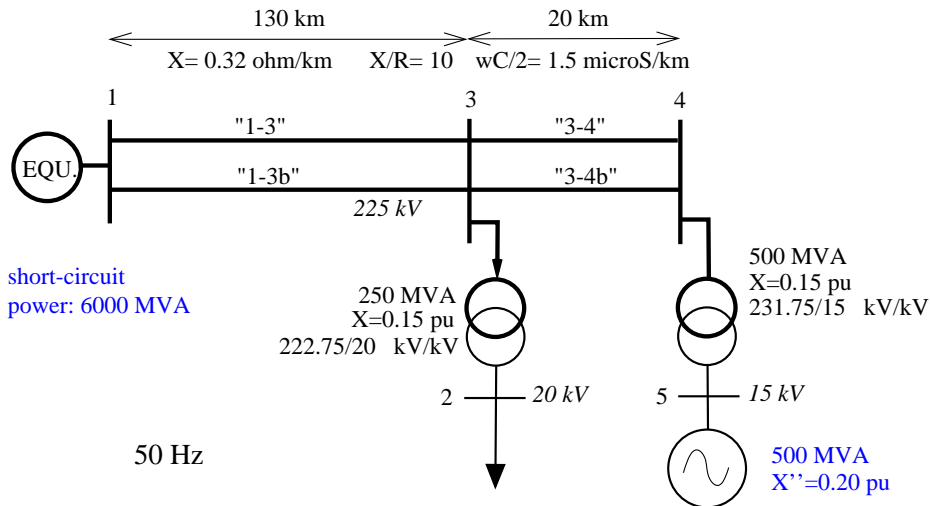
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# System modelling and operating points



## Load tap changer controlling voltage at bus 2

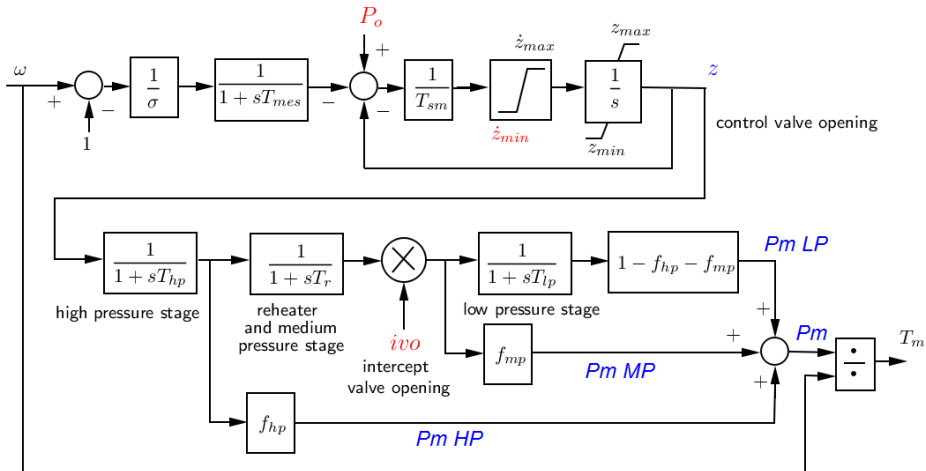
transformer ratio : minimum : 0.88                      maximum : 1.20  
 number of tap positions : 33  
 voltage dead-band :  $[V^o - 0.01 \quad V^o + 0.01] pu$   
 delay before first tap change : 25 s                      between subsequent tap changes : 10 s

## Generator G5: synchronous machine data

$$\begin{aligned}
 R_a &= 0. & X_\ell &= 0.15 pu & m &= 0.10 & n &= 6.0257 \\
 X_d &= 2.20 & X'_d &= 0.30 & X''_d &= 0.20 pu \\
 X_q &= 2.00 & X'_q &= 0.40 & X''_q &= 0.20 pu \\
 T'_{do} &= 7.00 & T''_{do} &= 0.05 & T'_{qo} &= 1.50 & T''_{qo} &= 0.05 s \\
 & & & & H &= 4 s
 \end{aligned}$$

(values in pu on the generator 500 MVA base)

## Generator G5: speed governor and steam turbine

 $P_{nom} = 460 \text{ MW}$ 

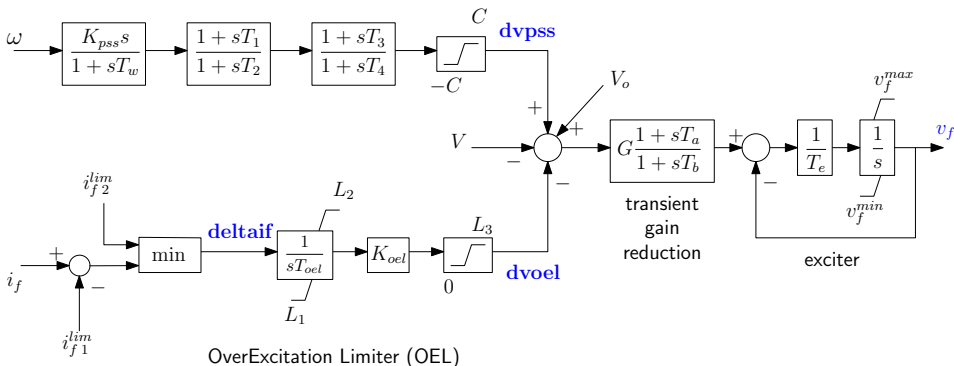
$$\sigma = 0.04 \quad T_{mes} = 0.1 \text{ s} \quad T_{sm} = 0.4 \text{ s}$$

$$\dot{z}_{min} = -0.05 \text{ pu/s} \quad \dot{z}_{max} = 0.05 \text{ pu/s} \quad z_{min} = 0. \quad z_{max} = 1. \text{ pu}$$

$$T_{hp} = 0.3 \text{ s} \quad f_{hp} = 0.4 \quad T_r = 5.0 \text{ s} \quad f_{mp} = 0.3 \quad T_{lp} = 0.3 \text{ s} \quad ivo = 1$$

## Generator G5: automatic voltage regulator, excitation system, overexcitation limiter

Power System Stabilizer (PSS)



OverExcitation Limiter (OEL)

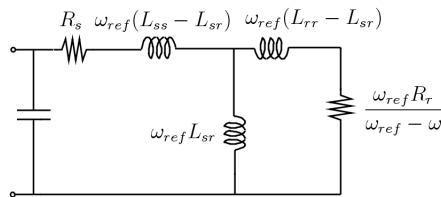
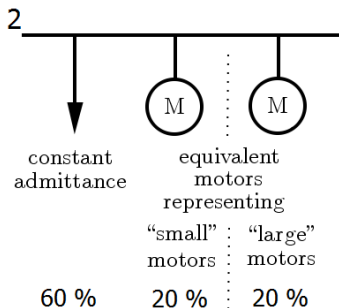
$$G = 70. \quad T_a = T_b = 1 \text{ s} \quad T_e = 0.4 \text{ s} \quad v_f^{min} = 0. \quad v_f^{max} = 5 \text{ pu}$$

$$K_{pss} = 50 \quad T_w = 5 \text{ s} \quad T_1 = T_3 = 0.323 \text{ s} \quad T_2 = T_4 = 0.0138 \text{ s} \quad C = 0.06 \text{ pu}$$

$$i_{f1}^{lim} = 2.90 \text{ pu} \quad i_{f2}^{lim} = 1.00 \text{ pu} \quad T_{oel} = 8 \text{ s} \quad K_{oel} = 2.0$$

$$L_1 = -1.1 \quad L_2 = 0.1 \quad L_3 = 0.2 \text{ pu}$$

## Modelling of load at bus 2



Mechanical torque:  $T_m = T_{mo}(A\omega^2 + B)$

“small motors”:

$$R_s = 0.031 \quad L_{ss} = 3.30 \quad L_{sr} = 3.20 \quad L_{rr} = 3.38 \quad R_r = 0.018 \text{ pu}$$

$$H = 0.7 \text{ s} \quad A = 0.5 \quad B = 0.5$$

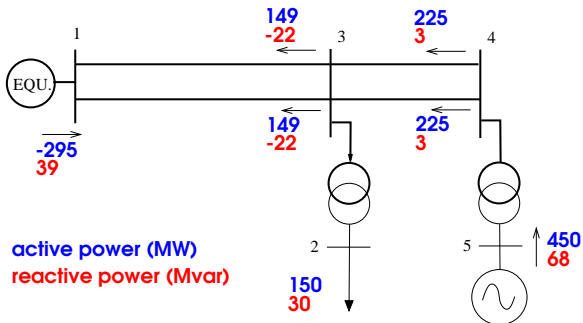
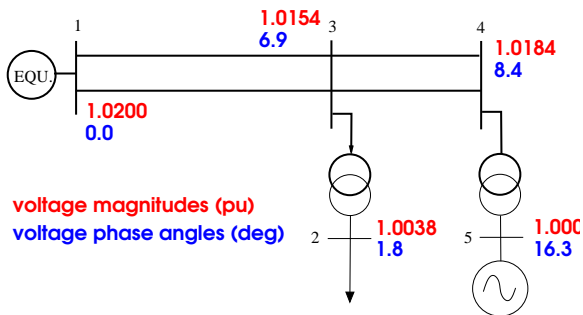
“large motors”:

$$R_s = 0.013 \quad L_{ss} = 3.867 \quad L_{sr} = 3.80 \quad L_{rr} = 3.97 \quad R_r = 0.009 \text{ pu}$$

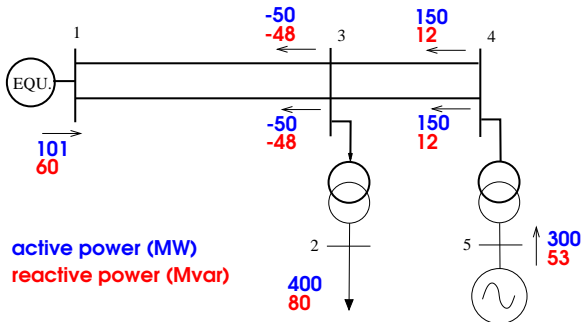
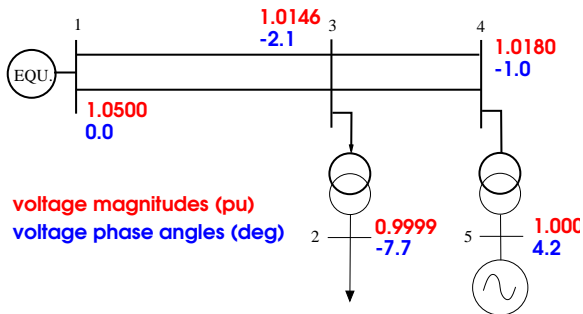
$$H = 1.5 \text{ s} \quad A = 0.5 \quad B = 0.5$$

(values in pu on the motor MVA base)

## Operating point # 1



## Operating point # 2





# Syntax of disturbance file

```
0.000 CONTINUE SOLVER BD 0.010 0.001 0.0 ALL
! add your events here, by increasing order of times.
20.000 STOP
```

To increase the power setpoint of generator G by D pu in T seconds :

```
<time> CHGPRM TOR G Po value_of_D value_of_T
```

To increase the voltage setpoint of generator G by D pu in T seconds :

```
<time> CHGPRM EXC G Vo value_of_D value_of_T
```

To increase the value of the Thévenin voltage by D pu in T seconds :

```
<time> CHGPRM INJ EQUIV1 ETH value_of_D value_of_T
```

To apply a fault at bus B with resistance R and reactance X (in  $\Omega$ , can be zero) :

```
<time> FAULT BUS B value_of_R value_of_X
```

To clear a fault at bus B :

```
<time> CLEAR BUS B
```

To trip line XYZ:

```
<time> BREAKER BRANCH XYZ 0 0
```

# Case 1

- Operating point : # 2
- disturbance : at  $t = 1$  s, increase of power set-point  $P_o$  by 115 MW in  $10 \text{ s}^{-1}$
- simulated time : 60 s.

Comment as far as possible the evolution of :

- the generator active power
- the generator reactive power
- the generator rotor angle
- the generator field current
- the control valve  $z$  of the turbine
- the voltage magnitude at bus 3.

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<sup>1</sup>power ramping are much slower in real life !

## Case 2

- Operating point : # 1
- disturbance : at  $t = 1$  s, increase of voltage set-point  $V_o$  by 0.05 pu in 2 s
- simulated time : 60 s.

Comment as far as possible the evolution of :

- the voltage magnitude at bus 3. In particular, explain the three “spikes” with the help of the proper curves
- the generator active power
- the generator reactive power
- the generator field current.

## Case 3

- Operating point : # 1
- disturbance : at  $t = 1$  s, “voltage dip” in the external system simulated by a decrease of the Thévenin voltage by 0.20 pu during 0.04 s  
(*can be seen considered as an impulse response*)
- simulated time : 20 s.
  
- Observe the evolution of the rotor speed of the generator
- Observe the evolution of the PSS output  
(*select: generator G5 - observable of excitation control - dvpss*)
- take the Power System Stabilizer (PSS) out of service, simulate the same disturbance and compare the evolution of the rotor speed with the previous one
- observe the evolution of the voltage magnitude at bus 3 and comment on the similarity
- what is the period of the dominant oscillation ?

Put the PSS back in service !

## Case 4

- Operating point : # 1
- disturbance : at  $t = 1$  s, a solid fault on line 1-3, cleared after 4 cycles (0.08 s) by opening the faulted circuit. The fault takes place very near bus 3, so that it can be applied at bus 3
- simulated time : 20 s.

Comment as far as possible the evolution of :

- the terminal voltage of the generator
- the active and reactive powers of the generator
- the rotor speed of the generator
- the field voltage of the generator  
(*select: generator G5 - observable of excitation control - vf*)
- the active power consumed by the impedance load at bus 2
- the active power consumed by one of the motors at bus 2
- the speed of one the motors at bus 2.

From RAMSES outputs, determine the current in line 3-4 during the short-circuit. Consider the value just after fault occurrence, for security. Check this value with a simple circuit calculation involving the generator equivalent circuit.

# Case 5

- Operating point : # 2
- disturbance : at  $t = 1$  s, tripping of **both** circuits of line 1-3 (without fault)
- simulated time : 25 s.

Comment as far as possible the evolution of :

- rotor speed of G5
- active power produced by G5
- control valve opening  
(*select: generator G5 - observable of torque controller - z*)
- turbine mechanical power  
(*select: generator G5 - observable of torque controller - Pm ;  
in pu on the turbine nominal power*).

Compute the final rotor speed using a formula from primary frequency control.  
Comment on the accuracy and try improving it.

# Case 6

- Operating point : # 2
- disturbance : at  $t = 1$  s, a solid fault on line 1-3, cleared after 10 cycles (0.20 s) by opening the faulted circuit. The fault takes place very near bus 3, so that it can be applied at bus 3
- simulated time : 20 s.
  
- Observe that the voltage at bus 3 does not recover near 1 pu, but stays “locked” near  $0.84 \text{ pu}^2$ . Find which system component is responsible for this, with the help of the proper curves
- show that for some shorter fault duration (i.e. smaller than 0.20 s), the voltage does not stay “locked” at such a small value. Explain the underlying instability mechanism.

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<sup>2</sup>this is a totally unacceptable value ! The system is considered unstable

# Case 7

- Operating point : # 1
  - disturbance : at  $t = 1$  s, severe disturbance in the external system simulated by a decrease of the Thévenin voltage by 0.2 pu in 1 s (the voltage remains at its low value)
  - simulated time : 120 s.
- 
- Explain why the voltage at bus 3 drops so much after some time.