

*ELEC0047 - Power system dynamics, control and stability*

## Long-term voltage stability : generation aspects

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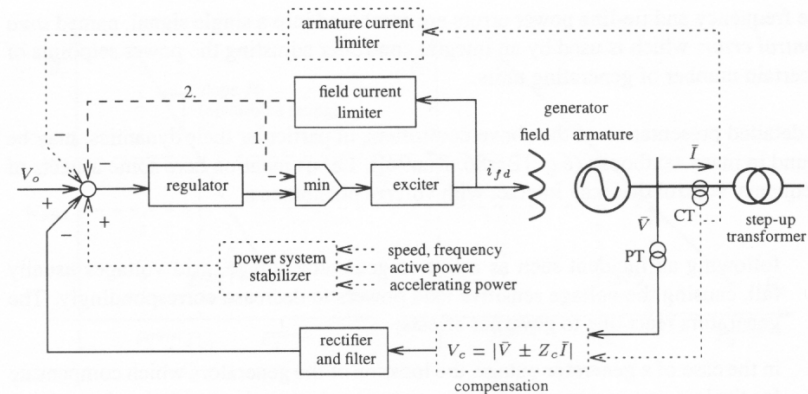
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*Voltage instability results from the inability of the combined transmission and generation system to provide the power requested by loads*

- Transmission aspects
- ▶ **Generation aspects**
- Load aspects

# Field and armature current limiters



- field current limit imposed by *OverExcitation Limiter* (OEL)
- armature (or stator) current limit: seldom enforced by a limiter; most often, action by operator in power plant.

# Generator QV curves

Region of admissible operating points in the  $(Q, V)$  plane, under constant  $P$

## Example of QV curves

50-Hz turbo-generator

rated apparent power: 1200 MVA

rated turbine power: 1020 MW

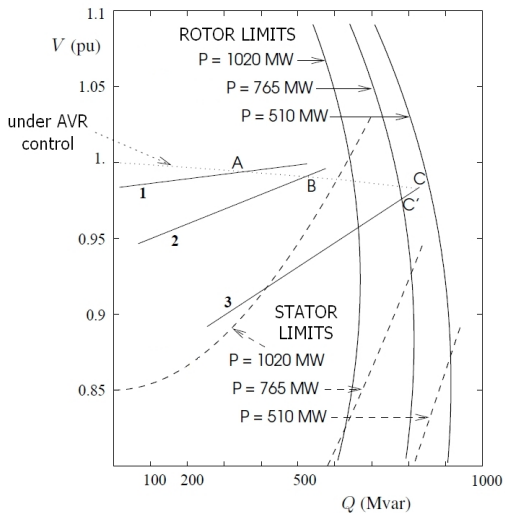
$X_d = 2.051$  pu

$X_q = 1.966$  pu

saturation taken into account

$I_f = 2671$  A at no load and nominal voltage

$I_f = 8300$  A after OEL activation



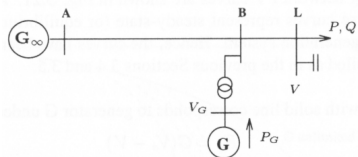
- Under Automatic Voltage Regulator (AVR) control:
  - there is a small voltage drop when the reactive power output increases
  - this is due to the proportional control used in AVR
    - a quite common choice
    - voltage drop is significant for low AVR open-loop static gain (e.g. 30-50 pu/pu)
  - in some other AVRs, integral control cancels the steady-state voltage error.
- Under rotor current limit :
  - assuming constant reactive power is an approximation : there is some variation with voltage
  - at least the reactive power limit must be updated with the active power  $P$  !

- Under stator current limit :

$$(V I_{max})^2 = P^2 + Q^2 \quad \Rightarrow \quad Q = \sqrt{(V I_{max})^2 - P^2}$$

- very constraining at low voltage
- Extreme scenario: machine under limit  $\rightarrow V$  drops a lot  $\rightarrow$  generator tripped by undervoltage protection
  - imposed by proper operation of power plant auxiliaries
  - acts for  $V \simeq 0.85 - 0.9$  pu
  - causes to lose *both*  $P$  and  $Q$  productions ! Larger cascading effects !

## Effect of generator reactive limits on maximum load power

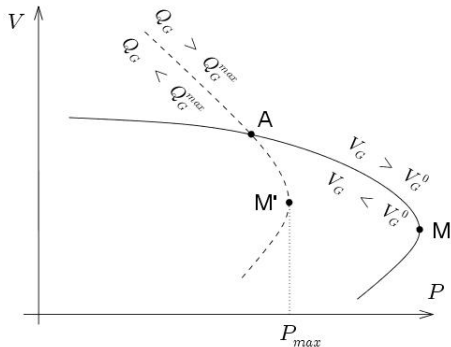


$G$  closer to  $L$  than  $G_\infty$

$P_G$  remains constant

$G$  controls  $V_G$  as long as  $Q_G \leq Q_G^{max}$

simple PV/PQ model used for  $G$



- When accounting for the reactive power limit, the maximum load power :
  - is reached at point  $M'$ , not  $M$  !
  - is significantly reduced
  - is generally reached at a higher voltage (more dangerous)
- in most cases voltage stability would not be a problem if generators were **un**limited sources of reactive power (i.e. constant voltage sources)
- need for reactive power reserves near the load centers
- impact of  $Q$  limit on max  $P \rightarrow$  electrical decoupling does no longer hold !

# Illustration with a power flow calculation

$$X_{AB} = 0.2, X_{BL} = 0.005, X_{GB} = 0.02 \text{ pu}, r_{GB} = 1.04, B_L = 200 \text{ Mvar}$$

$$P_L = 900, P_G = 400 \text{ MW}, Q_L = 200, Q_G^{max} = 250 \text{ Mvar}, V_G = 1.04, V_A = 1.05 \text{ pu}$$

Operating point beyond maximum load power

Trace of Newton iterations:

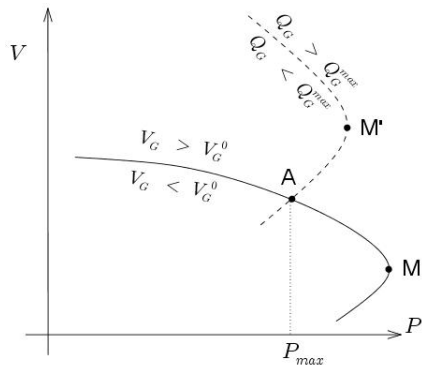
iter	max mismatches :	MW	Mvar
1		900.0	445.3
2		199.3	339.1
3		23.7	28.2
4		2.4	1.4
5		0.8	0.4
6		0.3	0.2
Gener G :	Q =	457.8 > Qmax =	250.0. Switched to PQ type
6		0.3	207.8
7		50.0	22.3
8		258.6	19.2
9		140.2	11.3
10		304.6	37.6

divergence of Newton iterations after the generator reactive limit is enforced.

# Effect of generator reactive limits - another situation

Same system

respective position of the PV curves is different



The maximum load power:

- is not reached at point M, where reactive capability of  $G$  is exceeded (would cause the OEL to act)
- is not reached at point  $M'$ , where generator voltage  $V_G$  is higher than setpoint  $V_G^0$  (would cause the AVR to regain control)
- is reached at the *breaking point* A, where  $V_G = V_g^0$  **and**  $Q_G = Q_G^{max}$



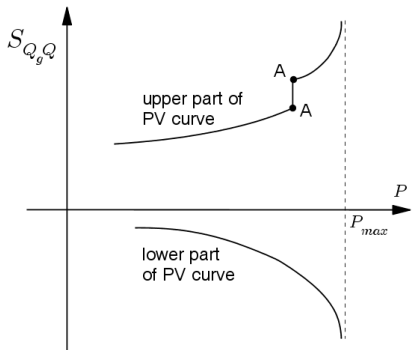
# Illustration with a power flow calculation

same data except  $Q_G^{max} = 350$  Mvar

iter	max mismatches :	MW	Mvar	
1		900.0	445.3	
2		199.3	339.1	
3		23.7	28.2	
4		2.4	1.4	
5		0.8	0.4	
6		0.3	0.2	
Gener G : Q = 457.8 > Qmax = 350.0. Switched to PQ type				
6		0.3	107.8	
7		13.1	5.0	
8		5.0	0.4	
9		0.2	0.1	dQg/dQl = -2.22 at bus L
Volt of gener G = 1.1418 > setpoint = 1.0500. Back under volt ctl				
9		32.2	496.0	
10		20.6	43.3	
11		1.7	1.5	
12		0.5	0.4	
13		0.2	0.1	dQg/dQl = 2.46 at bus L
Gener G : Q = 458.4 > Qmax = 350.0. Switched to PQ type				
13		0.2	108.4	
14		13.1	5.0	
15		5.1	0.5	
16		0.2	0.1	dQg/dQl = -2.22 at bus L
Volt of gener G = 1.1418 > setpoint = 1.0500. Back under volt ctl				
16		32.2	496.0	
17		20.6	43.3	
18		1.7	1.5 ...	

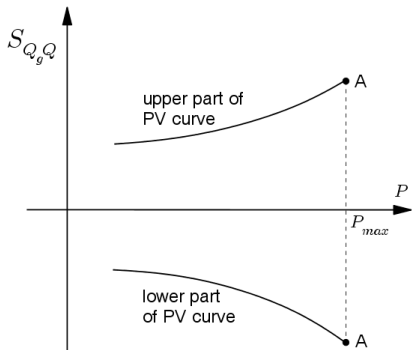
# Sensitivity behaviour in the presence of generator limits

Discontinuities at the points where a generator limit is enforced



case of slide 6

the sensitivity  $S_{Q_g Q}$  goes to infinity when passing through the maximum load power point



case of slide 8

the sensitivity  $S_{Q_g Q}$  does **not** go to infinity when passing through the maximum load power point