

ELEC0014 - Introduction to power and energy systems

# The "per unit" system

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 $\frac{\text{value of a quantity in physical unit}}{\text{value of corresponding "base" in same unit}} = \text{value of quantity in per unit (pu)}$ 

Advantages:

• the parameters of devices with similar design have close values in per unit, whatever the power of the device, provided they are referred to that power

 $\Rightarrow$  check of data validity is easier

 $\Rightarrow$  default values can be substituted to unavailable parameters

- in normal operating conditions, voltages in per unit are close to one
   ⇒ better conditioning of numerical computations
- the ideal transformer present in the model of a real transformer disappears after converting the parameters in per unit.

It is known that the internal reactance of a synchronous machine lies typically in the range  $[1.5 \ 2.5]$  pu (on the machine base)

• A machine with the characteristics (20 kV, 300 MVA) has a reactance of 2.667  $\Omega.$  Is this a normal value ?

We will see that the base impedance is  $20^2/300 = 1.333 \Omega$ value of reactance in per unit = 2.667/1.333 = 2 pu $\Rightarrow$  quite normal value !

• Same question for a machine with the characteristics (15 kV, 30 MVA)

The base impedance is now  $15^2/30 = 7.5 \Omega$ value of reactance in per unit = 2.667/7.5 = 0.356 pu  $\Rightarrow$  abnormal small value !

## Converting a simple circuit in per unit

Converting an electric circuit in per unit  $\implies$  choosing 3 base quantities

for instance: power  $S_B$  voltage  $V_B$  time  $t_B$ 

The other base values are obtained using fundamental laws of Electricity:

base current: 
$$I_B = \frac{S_B}{V_B}$$
  
base impedance:  $Z_B = \frac{V_B}{I_B} = \frac{V_B^2}{S_B}$   
base magnetic flux:  $\psi_B = V_B t_B$   
base inductance:  $L_B = \frac{\psi_B}{I_B} = \frac{V_B^2 t_B}{S_B}$   
base angular frequency:  $\omega_B = \frac{Z_B}{L_B} = \frac{1}{t_B}$ 

 $V_B$ ,  $I_B$ : RMS values.

### Variant (adopted in this course)

Consider an AC circuit operating at frequency  $f_N$ .

Choosing a base angular frequency instead of a base time:

$$\omega_B=\omega_N=2\pi f_N$$
 rad/s

from which one derives:

$$t_B = rac{1}{\omega_B} = rac{1}{\omega_N} = rac{1}{2\pi f_N}$$
 s

With this choice:

$$X_{pu} = \frac{X}{Z_B} = \frac{\omega_N L}{\omega_B L_B} = \frac{L}{L_B} = L_{pu}$$

At frequency  $f_N$ , the reactance and the inductance have the same per unit value!

### Converting in per unit a typical sinusoidal relation

In MVA, MW and Mvar:

$$S = V I \cos(\theta - \psi) + j V I \sin(\theta - \psi)$$

In per unit:

$$S_{pu} = \frac{S}{S_B} = \frac{VI}{V_B I_B} \cos(\theta - \psi) + j \frac{VI}{V_B I_B} \sin(\theta - \psi)$$
$$= V_{pu} I_{pu} \cos(\theta - \psi) + j V_{pu} I_{pu} \sin(\theta - \psi)$$

Same equation in physical units and in per unit !

In the above steady-state equation, time does not appear explicitly. Hence, only  $S_B$  and  $V_B$  are used.

### Converting in per unit a typical dynamic equation

In volts:

$$v = R i + L \frac{d i}{d t}$$

In per unit:

$$v_{pu} = \frac{v}{V_B} = \frac{R\,i}{Z_B\,I_B} + \frac{L}{\omega_B\,L_B\,I_B}\frac{d\,i}{d\,t} = R_{pu}i_{pu} + L_{pu}\frac{1}{\omega_B}\frac{d\,i_{pu}}{d\,t} = R_{pu}i_{pu} + L_{pu}\frac{d\,i_{pu}}{d\,t_{pu}}$$

In the above equation, time appears explicitly. There are two options:

- all variables, including time, are converted in per unit
  - $\longrightarrow$  identical equations in physical units and in per unit
- time is kept in seconds
  - $\rightarrow$  there appears a factor  $1/\omega_B$  in front of the derivation operator.

# Converting in per unit two magnetically coupled circuits

Flux-current relations:

$$\psi_1 = L_{11}i_1 + L_{12}i_2$$
  
$$\psi_2 = L_{21}i_1 + L_{22}i_2$$

Identical times. For reasons of simplicity we take:  $t_{1B} = t_{2B}$ 

Symmetry of inductance matrices. In Henry, one has:  $L_{12} = L_{21}$ . We want that this property still holds true in per unit.

$$\psi_{1pu} = \frac{\psi_1}{\psi_{1B}} = \frac{L_{11}}{L_{1B}} \frac{i_1}{l_{1B}} + \frac{L_{12}}{L_{1B}} \frac{i_2}{l_{1B}} = L_{11pu} i_{1pu} + \underbrace{\frac{L_{12} l_{2B}}{L_{1B} l_{1B}}}_{= L_{12pu}} i_{2pu}$$

Similarly for the second circuit:

$$L_{21pu} = \frac{L_{21}I_{1B}}{L_{2B}I_{2B}}$$

$$L_{12pu} = L_{21pu} \quad \Leftrightarrow \quad \frac{I_{2B}}{L_{1B}I_{1B}} = \frac{I_{1B}}{L_{2B}I_{2B}} \quad \Leftrightarrow \quad S_{1B} t_{1B} = S_{2B} t_{2B} \quad \Leftrightarrow \quad S_{1B} = S_{2B}$$

A per unit system preserving symmetry of inductance matrices is called *reciprocal*.

#### Summary

circuit $\# 1$	circuit # 2	
$S_B$	S <sub>B</sub>	$\leftarrow$ one degree of freedom
$t_B$	t <sub>B</sub>	$ =1/\omega_N$
$V_{1B}$	$V_{2B}$	$\leftarrow$ one degree of freedom in each circuit

Application to a network including several voltage levels connected through transformers:

- the same base power  $S_B$  is taken at all voltage levels. Usual value in transmission systems: 100 MVA
- the same base time  $t_B$  is taken everywhere (not used in steady state)
- at each voltage level, the base voltage is chosen in relation with the nominal voltage of the equipment.

# Converting in per unit a three-phase circuit

- Same base time  $t_B$  and same base power  $S_B$  everywhere
- at each voltage level, a base  $V_B$  is chosen for all phase-to-neutral voltages.

### 1st case. Unbalanced operation - analysis of the three phases

Convenient choice:  $S_B = \text{single-phase}$  power

$$ightarrow$$
 base current:  $I_B = \frac{S_B}{V_B}$   
ightarrow base impedance:  $Z_B = \frac{V_B}{I_B} = \frac{V_B^2}{S_B}$  etc.

Example. Convert in per unit the expression of the three-phase complex power:

$$S = \bar{V}_{a} \bar{I}_{a}^{\star} + \bar{V}_{b} \bar{I}_{b}^{\star} + \bar{V}_{c} \bar{I}_{c}^{\star}$$
$$S_{pu} = \frac{S}{S_{B}} = \frac{\bar{V}_{a}}{V_{B}} \frac{\bar{I}_{a}^{\star}}{I_{B}} + \frac{\bar{V}_{b}}{V_{B}} \frac{\bar{I}_{b}^{\star}}{I_{B}} + \frac{\bar{V}_{c}}{V_{B}} \frac{\bar{I}_{c}^{\star}}{I_{B}} = \bar{V}_{a \, pu} \bar{I}_{a \, pu}^{\star} + \bar{V}_{b \, pu} \bar{I}_{b \, pu}^{\star} + \bar{V}_{c \, pu} \bar{I}_{c \, pu}^{\star}$$

Identical expressions in physical units and in per unit !

### 2nd case. Balanced operation - per phase analysis

Convenient choice:  $S_B =$ three-phase power

Example. Convert in per unit the expression of the three-phase complex power:

$$S = \bar{V}_{a} \bar{I}_{a}^{\star} + \bar{V}_{b} \bar{I}_{b}^{\star} + \bar{V}_{c} \bar{I}_{c}^{\star} = 3 \bar{V}_{a} \bar{I}_{a}^{\star}$$
$$S_{pu} = \frac{S}{S_{B}} = \frac{3 \bar{V}_{a} \bar{I}_{a}^{\star}}{3 V_{B} I_{B}} = \bar{V}_{a pu} \bar{I}_{a pu}^{\star}$$

- All calculations are performed in a single phase, and in per unit
- **②** at the end, the power in all three phases is obtained by multiplying the power in per unit by  $S_B$ .

## Change of base

In a three-phase circuit, an impedance Z (in ohm) becomes in per unit

in the first base: 
$$Z_{pu1} = \frac{Z}{Z_{B1}} = \frac{Z S_{B1}}{3V_{B1}^2}$$
  
in the second base:  $Z_{pu2} = \frac{Z}{Z_{B2}} = \frac{Z S_{B2}}{3V_{B2}^2}$ 

Hence the formula to change from the first to the second base is:

$$Z_{pu2} = Z_{pu1} \frac{S_{B2}}{S_{B1}} \left(\frac{V_{B1}}{V_{B2}}\right)^2$$